

Highly flexible and transparent film heaters based on polyimide films embedded with silver nanowires†

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Highly flexible and transparent film heaters (TFHs) with superior mechanical and thermal stability were fabricated by embedding silver nanowires (AgNWs) into transparent polyimide (PI) films using a solution coating method. The fabricated AgNW/PI hybrid TFHs exhibited higher heating temperatures ($\sim 96^\circ\text{C}$) with lower input voltage ($\sim 6\text{ V}$), shorter response time ($T < 40\text{ s}$), and lower power consumption ($160.6^\circ\text{C cm}^2\text{ W}^{-1}$) than ITO/FTO heaters, as well as stability after repeated use. The AgNW/PI hybrid TFHs also showed excellent resistance to bending. After undergoing outer bending for a 1000 times, the change of sheet resistance was less than 18%. The effective embedment of the AgNW network in the surface of the transparent PI film not only decreased the surface roughness ($R_{\text{rms}} < 1\text{ nm}$) but also enhanced the resistance against oxidation and moisture. Potential applications of the AgNW/PI TFHs in window defogging and thermochromics are demonstrated.

1 Introduction

Transparent film heaters (TFHs) have attracted much attention for a wide range of applications including outdoor displays, defogging windows, and thermal-based sensors.^{1–5} A typical commercial film-like heater is a metallic wire made from an Fe–Cr–Al-based alloy.⁶ However, this alloy is rigid and has a low heating efficiency. A patterned copper foil thin film is another kind of commercial metallic film heater, which also suffers from similar shortcomings.⁷ A tin-doped indium oxide (ITO) transparent conductive film has been widely used as a heating element because of its high optical transmittance in the visible region, high electrical conductivity, and stability in environmental conditions.^{8–10} However, ITO is considered prohibitive, particularly in large area and flexible applications, because of indium scarcity, crack formation under mechanical bending, and slow thermal response.^{11–15}

Several electrical conductive materials, including carbon nanotubes,^{1,6,16} graphene^{17–19} and metal grids^{20–23} have been studied as possible alternatives to ITO. Used them as flexible TFHs, such materials should provide uniform thermal distribution over the heating area and reach higher temperatures at

low power.²⁴ Among the alternative materials, silver nanowires (AgNWs) have emerged as a promising candidate to fabricate TFHs because of their excellent conductivity, high transparency, and suitable mechanical properties.^{25–27} TFHs based on AgNWs have been reported.^{28–30} However, these reported TFHs are fabricated by depositing AgNWs onto the surface of a transparent polymer substrate, such as polyethylene naphthalate (PEN) or polyethylene terephthalate (PET). The relatively low thermal-resistance of PET or PEN limits the maximum temperature that the AgNW-based film heaters can reach. Moreover, the adhesion between AgNWs and substrate is weak, and the AgNW network on these substrates is no-resistant to scratches and can be easily detached from the substrates, resulting in low conductivity and inefficient heat production.

In this paper, fabrication of flexible TFHs comprising AgNW network embedded in the surface of transparent polyimide (PI) film is described. The AgNW/PI TFHs are developed to provide a combination of desirable properties including high glass transition temperature (T_g), mechanical flexibility, visual transparency, and strong bonding force with AgNWs. A TFH prepared from this composite generated a high saturation temperature up to 96°C , enabled rapid heating at lower operation voltages, and showed small temperature variation over prolonged period of heating at a constant voltage.

2 Experimental procedures

2.1 Materials

All reagents used in this study included silver nitrate (AgNO_3), poly(vinylpyrrolidone) (PVP, K-30), sodium chloride (NaCl),

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ethylene glycol (EG), acetone, ethanol, dianhydride, diamine, *m*-cresol, isoquinoline and *N,N*-dimethylacetamide (DMAc). All reagents were of analytical grade and purchased from Sino-pharm Chemical Reagent Co., Ltd. All chemicals were used as received without further purification.

2.2 Synthesis of transparent PI solution

The PI powder was first synthesized according to our previous studies.^{31,32} Dianhydride and diamine were used as monomers. Chemical structures of the monomers are shown in Fig. 1a. Typically, 4.0 mmol dianhydride, 4.0 mmol diamine, 15.0 mL *m*-cresol and 60 μ L isoquinoline were added into 50 mL flask and stirred in nitrogen at 190 $^{\circ}$ C for 10 h. Then the solution was diluted with *m*-cresol and slowly poured into a vigorously stirred ethanol. The precipitate was collected by filtration, washed with hot ethanol and dried. Photograph and chemical structures of the as-prepared PI powder are shown in Fig. 1b. In order to obtain homogenous PI solution, the PI powder was dissolved in DMAc with a weight percent of \sim 10% (ref. 33). Fig. 1c shows the photograph of the transparent PI solution.

2.3 Synthesis of AgNWs

Silver nanowires were fabricated using a modified polyol reduction. A PVP solution (50 mL 0.18 M in EG) was heated to 175 $^{\circ}$ C in a three-neck flask with stirring for 1 h. A NaCl solution (100 μ L 0.1 M in EG) was then added and stirred for 10 min. A AgNO₃ solution (50 mL 0.1 M in EG) was subsequently added to the flask dropwise at a rate of 5 mL min⁻¹. After AgNO₃ solution was added to the flask, the oil bath reaction lasted another 20 min. The clear solution changed color through yellow, red-orange, green, dark gray, and finally to glistening gray, which indicated the formation of long AgNWs. Then the solution was cooled to room temperature and was centrifuged (3 times at 2000 rpm) to remove solvent (EG), PVP and other impurities in the supernatant after adding acetone. After the final centrifuge, the AgNWs were redispersed in ethanol at a concentration of 0.3 mg mL⁻¹. The diameters of the AgNWs were in the range of 60 to 80 nm, and the lengths between 10 and 20 μ m (ESI, Fig. S1†).

2.4 Fabrication of AgNW/PI TFHs

Fig. 2a schematically illustrates the fabrication of the AgNW/PI TFHs. AgNW dispersion was rod-coated on a pre-cleaned rigid glass substrate with different cycles and dried on a hot plate for 3 min at 60 $^{\circ}$ C. Further, transparent PI solution was cast on the AgNW film and then placed in an oven at 80 $^{\circ}$ C for 2 h to evaporate most of the solvent and subjected to schedule heating at 100, 150, and 200 $^{\circ}$ C for 60 min at each temperature. Following the annealing, the resulting AgNW/PI TFHs with a thickness of \sim 50 μ m were peeled off and cut into various sample sizes. The entire process was realized in air. Fig. S2 (ESI†) shows the photograph of fabrication of 10 cm \times 10 cm flexible AgNW/PI TFH.

2.5 Characterization and measurement

The surface morphologies of AgNW/PI TFHs were examined using scanning electron microscopy (SEM, Hitachi S-4800). The surface roughnesses of AgNW/PI TFHs were examined using an atomic force microscope (AFM, Veeco Dimension 3100V). The optical transmittance of the transparent PI film and AgNW/PI TFHs were obtained at room temperature using an ultraviolet-visible spectrophotometer (Perkin-Elmer, Lambda 950, USA) with an integrating sphere. The sheet resistance of AgNW/PI TFHs was measured using a four-point probe system (Napson Corp. Cresbox). The DC voltage was supplied by a power supply to the TFHs through a copper contact at the film edge. The temperature of the TFHs was measured using an infrared thermometer (Smart Sensor, AR842A). In order to accurately reflect the thermal distribution, nine temperature points were measured for each TFH. The average temperature was used in

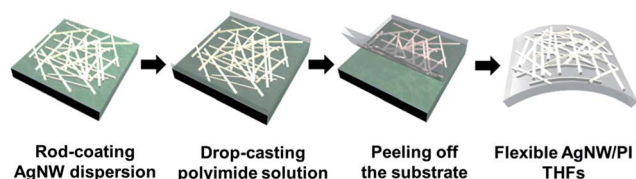


Fig. 2 Fabrication process of the AgNW/PI TFHs.

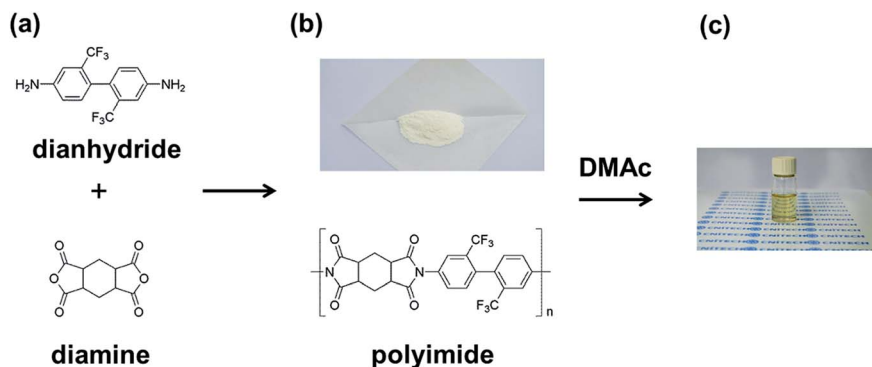


Fig. 1 Synthesis of PI solution. (a) Chemical structures of the monomers employed. (b) A photograph and chemical structure of the as-prepared polyimide powder. (c) A photograph of the PI solution.

our experiment. The mechanical stability tests were performed using a lab-made bending test machine. The moisture test was carried out at a temperature of 121 °C, a relative humidity (RH) of 97%, and a gauge pressure of 0.1 MPa using highly-accelerated temperature and humidity stress test (HAST, PC-422R8, Hirayama). The adhesion test was performed using 3M stock tape.

3 Results and discussion

3.1 Surface morphologies of AgNW/PI TFHs

SEM images of AgNW/PI TFHs with different numbers of AgNW rod-coating cycles (N) are shown in Fig. 3. The density of the AgNWs in the TFHs increased with increasing numbers N . In addition, the TFHs had a well-connected wire-to-wire junction and smooth surface, unlike the forest-like AgNW structure observed in pure AgNW films. The AgNWs were inlaid in the surface of the TFHs. No void was observed on the surface, indicating that all AgNWs had been transferred into the surface of the PI film. The AgNW/PI TFH displayed a smooth surface with a mean surface roughness of 0.4 nm, as can be seen from the AFM images in Fig. 3c and d. This surface morphology indicates that the transparent PI solution permeated the AgNWs network well and filled the holes in the networks, as well as the voids at the interface between AgNW and the rigid substrate.

3.2 Optical and electrical properties of AgNW/PI TFHs

The optical transmittance spectra of the TFHs with increasing numbers N are shown in Fig. 4, and the sheet resistance values

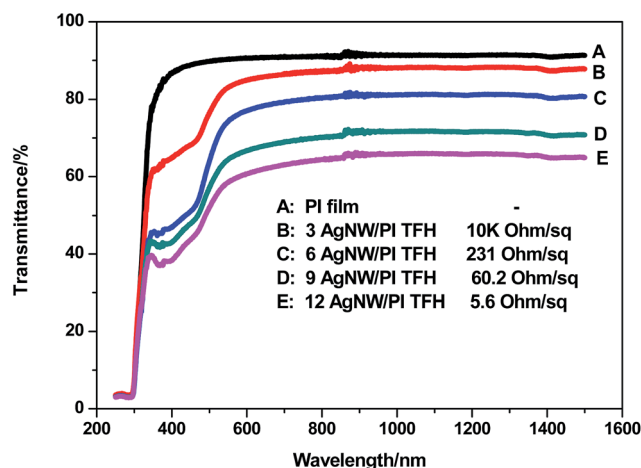


Fig. 4 Optical transmittance spectra of the pure PI film and TFHs, and the relationship between sheet resistance and the number of rod-coating cycles of TFHs.

of each TFH are also given. The pure PI film displayed a high optical transmittance of 90.2% at 550 nm. When the AgNWs were inserted, the transmittance of TFHs decreased as the number of N increased. This change was caused by the light reflection and scattering from the AgNWs. Moreover, the sheet resistance of the TFHs decreased as N increased. The 3AgNW/PI ($N = 3$) sample displayed a sheet resistance of 10×10^3 Ohm sq^{-1} with a transmittance of 82.8% at 550 nm, whereas the 12AgNW/PI ($N = 12$) sample displayed a sheet resistance of 5.6 Ohm sq^{-1} with a transmittance of 58.1% at 550 nm. The results

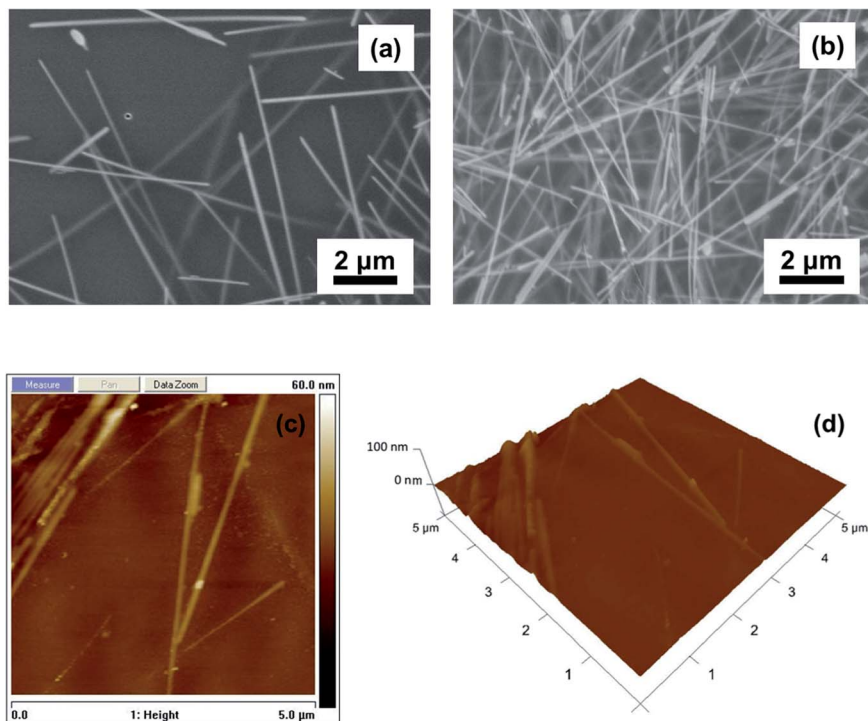


Fig. 3 SEM images of AgNW/PI TFHs with different rod-coating cycles of AgNW: (a) $N = 3$ and (b) $N = 12$. (c) 2D and (d) 3D AFM images of AgNW/PI TFHs ($N = 3$).

indicated that the AgNW density could be adjusted to optimize the optical and electrical properties of AgNW/PI TFHs.

3.3 Thermal response behavior of AgNW/PI TFHs

In order to understand the nature of Joule heating in the TFHs, the temperature properties of AgNW/PI TFHs were analyzed. The size of the AgNW/PI TFHs used in this section was $2.5\text{ cm} \times 2.5\text{ cm}$. Fig. 5a shows the temperature profiles of the TFH, which is plotted with respect to the input voltage (modulated from 1 V to 6 V). The optoelectronic performance of the TFH used was 5.6 Ohm sq^{-1} with a corresponding transmittance of 58.1% at 550 nm. All of the plots showed that the temperature of the TFH reached 29.9°C when the input voltage was set at 1 V. When the input voltage was increased to 6 V, the temperature of the TFH reached above 96°C , confirming its good operation at a low input voltage. Higher power at a low input voltage implies an efficient transduction of electrical energy into Joule heating. The response time, which is defined as the time required to reach the steady-state temperature ($T_{\text{steady-state}}$) from room temperature (T_{room}), is one of the key factors for evaluating the performance of TFHs. Regardless of the applied voltage, the

increase in temperature was very fast, and the steady-state temperatures were reached in less than 40 s, demonstrating the fast response of the device.

Power consumption, which is defined as temperature increase per input electrical power, is also an important parameter for evaluating the heat performance. To examine the power consumption, Joule's law is used to determine the heat generated by a film heater

$$P = U^2/R \quad (1)$$

where P is input power, U is the applied voltage and R is the resistance of the film heater over which the voltage is applied. Fig. 5b shows input power as a function of the steady-state temperature. Based on the data shown in Fig. 5b and considering the size of the TFH, the electrical power consumption of the TFH was calculated and its value was approximately $160.6^\circ\text{C cm}^2\text{ W}^{-1}$.

The temperature-time curves remained unchanged and the maximum temperature slightly increased (Fig. 6). Stability tests under electrical stress at an applied bias for 1 h showed no significant degradation of achievable temperature, both of which manifested the stability for repeated and long-term use. The slight increase of the maximum temperature in Fig. 6 indicated that a slight decrease of heater resistance could be ascribed to more closely connected nanowires.

To investigate the thermal response of the fabricated AgNW/PI TFHs. The relationship between $T_{\text{steady-state}}$ and T_{room} of the AgNW/PI TFHs was expressed by the following equation:³⁴

$$T_{\text{steady-state}} = \frac{U^2/R - Q_d}{Cm} + T_{\text{room}} \quad (2)$$

where C is heat capacity ratio of the film, m is film mass, and Q_d is the heat dissipated from the film.

Heat dissipation (Q_d) involves heat transfer by radiation and convection. Radiation could be negligible at temperature below 150°C .³⁵ Air convection is the significant path of heat dissipation and $T_{\text{steady-state}}$ can be reached when Joule heating and convection reached a dynamic balance at the elevated temperature.

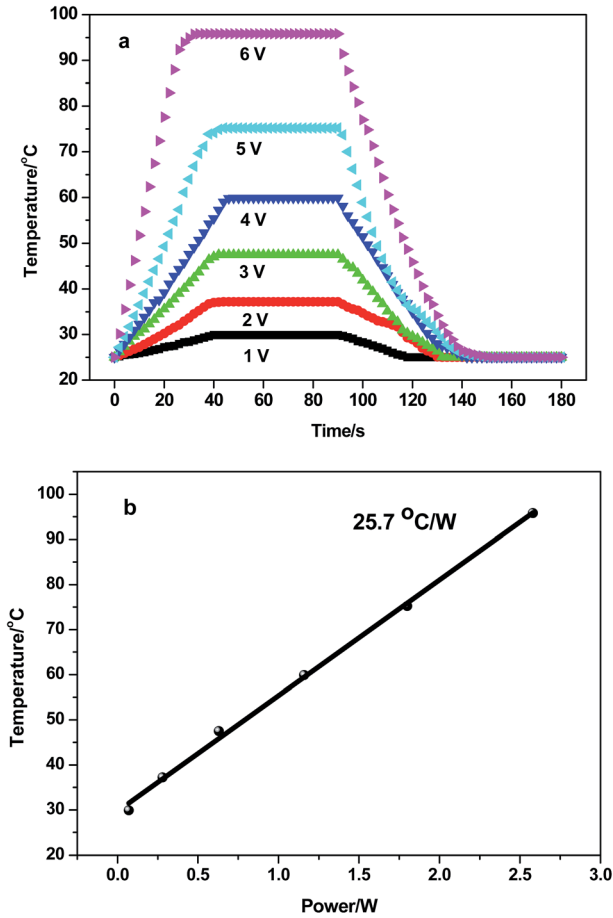


Fig. 5 (a) Temperature profiles of the AgNW/PI TFH with the sheet resistance of 5.6 Ohm sq^{-1} under its operation at different input voltages. (b) Input power as a function of the steady state temperature of the AgNW/PI TFH.

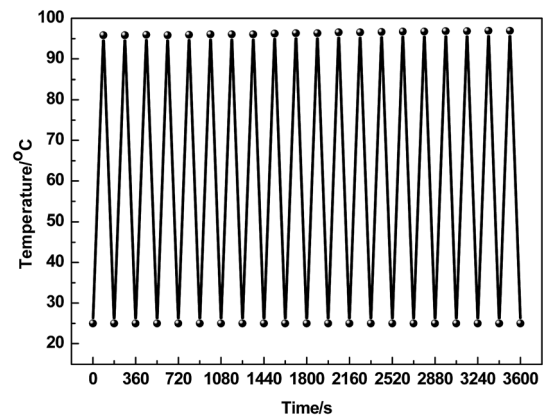


Fig. 6 Cycling performance of AgNW/PI TFH with sheet resistance of 5.6 Ohm sq^{-1} .

Eqn (2) shows that the $T_{\text{steady-state}}$ increases with the applied voltage U and decreases with decreasing resistance R , or the film heater's sheet resistance when the sample geometry is fixed. Under the same input voltage (6 V), the maximum temperature at steady state increased as the sheet resistance of the AgNW/PI TFHs decreased, which suggests that the sheet resistance value of the film should be less than 60 Ohm sq⁻¹ to afford a maximum temperature above 70 °C (ESI, Fig. S3†).

3.4 Mechanical behavior of AgNW/PI TFHs

In addition to the excellent surface morphology and thermal response behavior, AgNW/PI TFHs possesses superior mechanical flexibility, which is a desirable attribute for the emerging flexible electronic devices. Outer bending and inner bending tests were performed using a lab-made bending test system at a fixed bending radius of 5 mm operated as a function of the number of bending cycles (Fig. 7a and b). The nominal bending strain can also be calculated using the following equation:

$$\varepsilon_f = \frac{h}{2r}$$

where ε_f , h , and r are the nominal bending strain, substrate thickness, and bending radius, respectively. The typical bending strain in the study after calculation was 0.5%.

Fig. 7c shows the sheet resistance change in AgNW/PI TFHs. The change in film resistance can be expressed as $\Delta R = (R - R_0)/R_0$, where R_0 is the initial sheet resistance and R is the value measured after the bending test. Resistance changes were recorded for three times for each bending cycle to ensure accuracy of the measurement. The resistance changes were 0.16% and 0.305% for outer bending and inner bending tests, respectively. The electrical properties of AgNW/PI TFHs were more robust to both outer and inner bending, which is

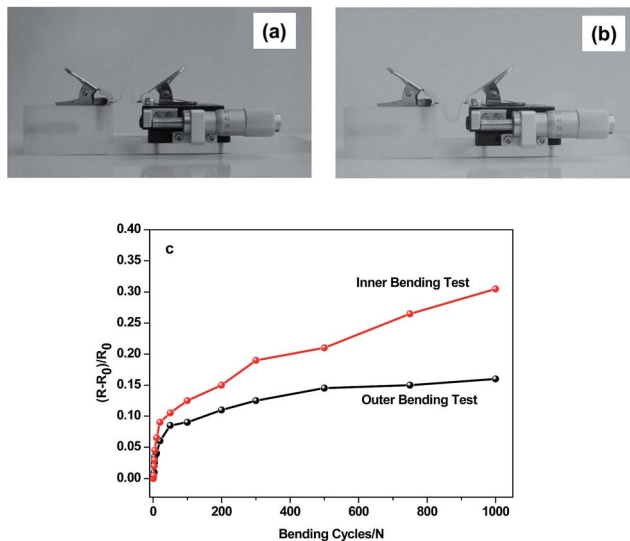


Fig. 7 Photograph of the laboratory-made (a) outer and (b) inner bending test machine used in this study. (c) Sheet resistance change of the AgNW/PI TFH.

attributed to the strong bonding between the transparent PI film and AgNWs network. Such strong bond could prevent sliding at the interface under extreme bending. We also observed change in the sheet resistance of the AgNW/PI TFHs under extreme conditions of folding and crumpling (ESI, Fig. S4†).

3.5 Moisture behavior of AgNW/PI TFHs

To confirm the long-term reliability of AgNW/PI TFHs, the optical and electrical performances of the AgNW/PI TFHs were evaluated in a humidity chamber (121 °C, 97% relative humidity for 24 h) for thermal moisture testing. Fig. 8a shows the optical and electrical properties of the AgNW/PI TFH before and after the thermal moisture testing. A slight decrease in transmittance ($T_{550, \text{before}} = 64.0\%$ and $T_{550, \text{after}} = 60.4\%$) was mainly due to the change of the PI film in the harsh environment. The increase in resistance was mainly due to oxidation of a small amount of AgNWs exposed on the surface of the AgNW/PI TFHs. Fig. 8b shows the thermal response of the AgNW/PI TFHs before and after the thermal moisture testing. $T_{\text{steady-state}}$ decreased from

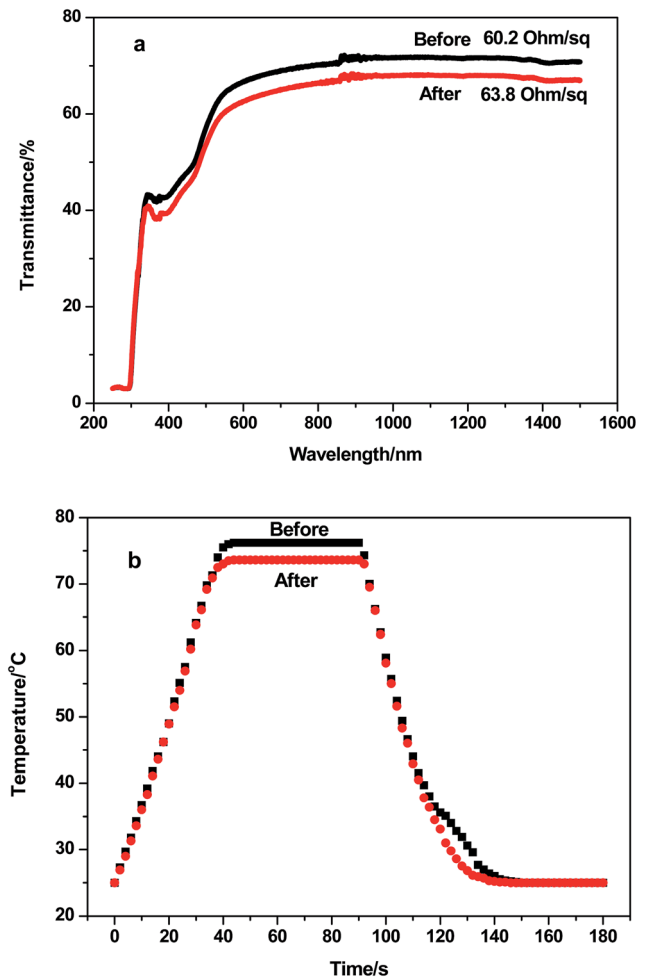


Fig. 8 (a) Optical and electrical properties of the AgNW/PI TFH before and after the thermal moisture test. (b) Thermal response of the AgNW/PI TFH before and after the thermal moisture testing.

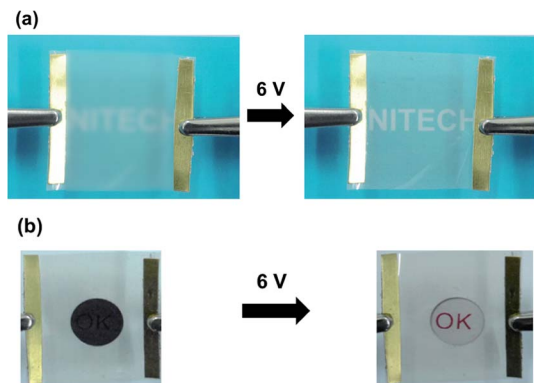


Fig. 9 Applications of the AgNW/PI TFHs: (a) defrosting test before and after operation at 6 V. (b) Thermochromic behavior of symbol with the AgNW/PI TFHs before and after operation at 6 V.

76.2 °C to 73.6 °C. Nearly stable heating temperature indicates that the AgNW/PI TFHs can be designed for defrosting window panel used in outdoor advertisement board.

Adhesion of the AgNW/PI TFHs was tested by repeated sticking and peeling. 3M Scotch tape was applied on the surface of the TFHs. After 1000 adhesion peeling cycles, the sheet resistance only increased by 0.057, indicating a strong bonding of the conductive nanowires on the TFHs (ESI, Fig. S5†).

3.6 Applications of AgNW/PI TFHs

Two potential applications of the AgNW/PI TFHs are demonstrated in Fig. 9. As shown in Fig. 9a, the AgNW/PI TFHs can be used as a defroster. Under the operating voltage of 6 V, the frost on the surface was completely removed within 60 s, making the logo of our institute clearly visible. Moreover, the AgNW/PI TFHs can be used as substrate to power thermochromic symbols (Fig. 9b and ESI, Fig. S6†). The thermochromic symbol had a switching temperature of 65 °C and was attached to the surface of the AgNW/PI TFHs. After applying a voltage of 6 V, the black symbol gradually became transparent, and the red “OK” became clear. After turning the voltage off at 90 s, the thermochromic symbol changed back to the original black color and the “OK” became blurred.

4 Conclusions

Flexible TFHs comprising AgNWs network embedded in the surface of transparent PI film was fabricated by a solution process. By adjusting the number of rod-coating cycles of the AgNW suspension, a typical AgNW/PI TFH with a low sheet resistance of 5.6 Ohm sq⁻¹, and a transmittance of 58.1% was obtained by adjusting the number of rod-coating cycles of the AgNW suspension. Thermal response tests of AgNW/PI TFH were performed to show higher heating temperature of 96 °C, a quick response time of less than 40 s, lower power consumption of 160.6 °C cm² W⁻¹, and stability for repeated use. The mechanical properties of AgNW/PI TFH were also investigated. The resistance changes were 0.16% and 0.305% for the outer bending and inner bending tests, respectively. In addition, the

AgNW/PI TFHs showed nearly stable optical property, sheet resistance and heating temperatures after testing in a humidity chamber under 121 °C/97% relative humidity for 24 h. As such, the fabricated AgNW/PI TFHs have potential applications in window defogging, thermochromics and transparent electrodes.

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